ELECTROLYTES FOR PLASMA ELECTROLYTIC OXIDATION OF MAGNESIUM

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Abstract

The classification of electrolytes for PEO treatment of magnesium is given. The probable mechanism for the formation of refractory compounds is considered. Several sealing methods are described. Some experimental results obtained on magnesium coted in silicate- and aluminate containing electrolytes are presented.

1. Introduction

In the literature devoted to plasma electrolytic oxidation (PEO) of magnesium, dozens of electrolyte compositions and electrical regimes are given [1]. At the same time, many publications contain sketchy information concerning electrolyte recipes connected with the characteristics of coatings. The absence of significant technological details in the description of the experiments did not allow us to analyse all the variety of works that appeared in recent years. This paper covers only those publications that contain a fairly complete description of the regimes, electrolytes, and chemical composition of the coatings obtained.

2. Typical electrolytes and coatings composition

At present, a number of universal solutions have been developed [2], suitable for plasma oxidation of both magnesium and aluminium (Table 1).

Components of electrolytes	Content, g.l ⁻¹		
and electrical regimes	Aluminium	Magnesium	
Na ₂ SiO ₃	3-10	0	
КОН	1-3	0-2	
$Na_2P_4O_7$	0-5	0-5	
NaF	0	2-7	
NaAlO ₂	0	4-10	
Time of electrolysis, min	<120	20	
Current density, A.m ⁻²	<2000	<1000	
Temperature, ⁰ C	10-	-40	
Thickness, µm	<70	<30	

Table 1. Electrolytes and regimes applicable for both aluminium and magnesium

According to the main component forming polymer anions, all known compositions can be classified into four groups: silicate, aluminate, phosphate and borate. Within each group, the composition of electrolytes can vary, for example, silicate-phosphate,

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aluminate-fluoride, etc. To adjust the pH, ammonia, alkalis and acids are usually added. To improve the uniformity of the coatings, organic and surface-active substances can be used.

Table 2 represents main conditions of electrolysis and composition of coatings obtained on different Mg alloys. These data were taken from publications that, in the opinion of the authors, contain the most complete information concerning the relationship between the composition of the electrolytes and t coatings.

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N⁰	Magnesi	Regime	Electrolyte, g.L ⁻¹		Coating	Refer
	um alloy	C:1			composition	ences
	T	511	icate electrolytes		1	1
1	AM60B	600 A.m ⁻²	KOH	1	MgO, KMgF ₃ ,	[3]
		Pulse regime	$Na_2SiO_39H_2O$	10	Mg_2SiO_4	
			KF	8	$MgAl_2O_{4,}$	
2	A721D	$400,000,4x^{-2}$	KOU	2	MgF_2	Г <i>4</i> 1
2	AZ3ID	400-900 AM		3 15	MgO, Mg_2SIO_4	[4]
		f_{-} 700 H_{7}	$Na_2S1O_3 \cdot 9H_2O_6$	-15		
		1- /00 IIZ	$KF \cdot 2H_2O$	3		
2	A721D	$200 \text{ A} \text{ s}^{-2}$	$Na_2B_4O_7 \cdot 10H_2O$	4	Ma Sio Mao	[6]
3	AZ31B	300 AM ,		2	Mg_2S1O_4 , MgO	[5]
		Direct current	$Na_2S1O_3 \cdot 9H_2O$	0		
			AF Cluserel 1	2		
4	Μα	$400 \text{ A} \text{ m}^{-2}$		2.0	MarRio	[6]
4	(99.95%)	Direct	NasSiOs9HaO	160	$Mg_2D_2O_5$, Mg_2SiO_4	[0]
	()).))/()	current	Na ₂ B ₄ O ₇ 10H ₂ O	160	SiO_2	
		$t=1-22 \min$	110120	100	5102	
5	AZ91HP	400 Am^{-2}	NaOH	10	Amorphous	[7]
C		f=2000 Hz.	Na ₂ SiO ₃	18	structure, MgO	L'J
		duty cycle	NaOH	10		
		20%,	$C_6H_{18}O_{24}P_6$ (p)	hytic		
		t=3 min	acid) 12	•		
6	AZ31	Pulsed	Na ₂ SiO ₃	10	MgO, MgAl ₂ O ₄ ,	[Erro
		current, t=70	Na ₂ WO ₄ , KOH,		MgSiO ₃	r!
		min	Na ₂ EDTA			Book
						mark
						not
						defin
-		-2				ed.8]
1	Mg	650 A.M ²	Na ₂ SiO ₃ (ρ	=1.5	MgO, Mg ₂ S ₁ O ₄	[Erro
	(99.9%),	rectangular	g.cm [°])	57.5		r! Deele
	AZ51,	puises,	$Na_4P_2O_7.10H_2O$	15		BOOK
	$\Delta 701D$	current				not
	7C71	$i_{a}/i_{a}=1.2$				defin
	ZE41	f = 50 Hz				ed.91
	WE43-T6	t=15 min				
8	AZ91D	3-5 A	Na ₂ SiO ₃	15	MgAl ₂ O ₄	[10]
		f= 500Hz	NaOH	3		

Table 2. Electrolytes and regimes for PEO of magnesium alloys

9	AZ91D	AC mode 50	$Na_2SiO_3 0$	$.05 \text{ mol.L}^{-1}$	Mg, O	[11]
		Hz $10.0 \text{ A} 1^{-2}$	KOH 0.04 mol.L^{-1}			
		10.0 A.dm	KF 0-0.1	2 mol.L		
		t=60 min				
10	AZ31B	1000 A.m^{-2}	Na ₂ SiO ₃	6	Mg ₂ SiO ₄	[12]
			KF	2	TiO_2 (rutile and	
			КОН	2	anatase)	
			Glycerol	12.61	MgO	
			Surfactant	(sodium	Mg	
			dodecyl	sulphate,		
			diphenylai	mine 4-		
			sulphonate	e or sodium		
			dodecyipn			
11	Δ731	Bipolar	NasSiOa	0.23	Μα	[13]
11	ALS1	pulses	KF	3 2	MgO	[13]
		$i_a=i_c=350$	КОН	20	Mg ₂ SiO ₄	
		Am^{-2}	Glycerol	12.61	11920104	
		duty cycle	5			
		10-40%,				
		f=600 Hz				
		t=30 min				
12	AZ91D	Bipolar	Na ₂ SiO ₃ 9I	H ₂ O 6-15	MgO 41%	[4]
		pulses f=700	$Na_2B_4O_71$	$0H_2O4$	Mg_2SiO_4	
		Hz, 60 V	КОН	3	59%	
10		1.50.250	KF_2H_2O			503
13	AZ91D	150-250	KOH	10	MgO Mg(OII)	[9]
		A.m	K_2S1O_3	10	$Mg(OH)_2$	
14	A701D	U- 500 V	Na SiOa	15	MgSIO ₃	[1/]
14	AL/ID	$f_{-} = 600 \text{ Hz}$	NaOH	10	Mg ₂ SiO ₄	[14]
		duty cycle	KF	8	TiO_2	
		8%.	Glycerol	6.3	1102	
		t=5 min	Titanium	sol		
			to 1			
		Alu	minate elect	rolytes		
15	Al 2-12,	40 A.m^{-2}	KOH	168	MgAl ₂ O ₄	[15]
	Mg rest	Direct current	Na_3PO_4	4.44	γ -Al ₂ O ₃	
			KF N A1O	34.8		
16	A 701D	100 1	NaAlO ₂	32.8-90.2		[16]
10	ALYID	Direct current	KF	5-15 0-15	$M_{\sigma}\Delta l_{\sigma}\Omega$	[10]
17	A 162	Monopolar	NaAlO ₂	10-10	MgAl ₂ O ₄	[17]
1	11002	pulses. duty	1102	10 20	1,161 11204	
		cvcle - 80%.				
		f= 2 кHz;				
		t=10-20 min				
18	Magnesium	Keronite [®]	Keronite®	(Na ₂ SiO ₃	MgO	[18]
	alloy wire			-,	$MgAl_2O_4$	

	(2% Al, 1%	Bipolar	NaOH, Na ₃ PO ₄)		MgO	
	Zn,	pulses,	, , ,		Al_2O_3	
	0.2% Mn)	200-100				
	,	$A.m^{-2}$				
		$\tau = 3.5 - 7 \min$				
		f=1000 Hz				
19	AZ91HP	70 -90 V,	КОН	165	MgO	[19]
	(Mg-9.Al-	200 - 5000	Al(OH) ₃	34	MgF ₂	
	1. Zn-allov)	$A.m^{-2}$	KF	34	02	
	,	$\tau = 10 \text{ min}$	Na_3PO_4	34		
		• • • • • • • • • • • • • • • • • • • •	KMnO ₄	20		
		Pho	sphate electro	olytes		
20	AZ91D	400-900	KOH	5	Mg	[4]
	-	$A.m^{-2}$	(NaPO ₃) ₆	5-15	MgO	
		Pulse current.	Na ₃ AlF ₆	5-10	8 -	
		f = 700 Hz	Triethanola	mine 4		
21	WE43	600 A.m^{-2}	КОН	1	ΜσΟ	[23]
	AZ91D	Pulse current	NaAlO ₂	8	MgAl ₂ O ₄	[=0]
			Na ₂ PO ₄	10	11-8-112 0 4	
22	A791D	50 A m^{-2}	KOH	168	ΜσΟ	[20]
		Direct current	Na ₂ PO ₄	4.44	Al ₂ O ₂	[20]
		Direct current	KF	34.8	$Al(OH)_2$	
			$Al(NO_2)_2$	32		
23	WF43-T6	300 A m^{-2}	Na ₂ PO ₄ 12H	$\frac{32}{167.7}$	ΜσΟ	[21]
23	A791D	Direct	NH4OH	52 56	$Mg_{2}(PO_{4})_{2}$	
		current	1114011	52.50	WI <u>G</u> 3(1 04)2	
		t - 2400 s				
24	AM50	420 V	Na ₂ PO ₄	8	$7r\Omega_{2}$	[22]
21	111150	t=10 min	NH ₄ OH	18	ΜσΟ	
		t=10 mm	K ₂ ZrE _c	3	MgE ₂	
			NaH ₂ PO ₂	1	101 <u>G</u> 1 2	
25	AM60B	70-80-90 V	KOH	3.0	ΜσΟ	[23]
20	1 Millood	Voltastatic	Na ₂ PO ₄	0.21	11190	[23]
		regime	$Al(NO_2)_2$	0.15		
		t=15 min	11(1103)3	0.12		
256	AM50	$300 \text{ A} \text{ m}^{-2}$	Ca(OH) ₂	2	ΜσΟ	[24 E r
200	1 11/10/0	Alternating		5-15	$Mg_2(PO_4)_2$	ror!
		nulses (2 ms)	11431 04	5 15	$CaH(PO_4)_2$	Book
		and nauses			CaO_2 (calcium)	mark
		(18 ms)			peroxide)	not
		t=15 min			r ····································	defin
		t=10 mm				ed.]
27	AZ31	$4 \mathrm{A.m^{-2}}$	$Ca(NO_2)_2$	6.9	Mg	[25]
		85-80 [°] C	NH ₄ H ₂ PO ₄	2.88	$Ca_{10}(PO_4) \in (OH)_2$	[_~]
		t = 60 min	NaNO ₂	13.9	CaHPO ₄ 2H ₂ O	
			HNO ₂ or	NH ₄ OH		
			(adjusting n	H = 5)		
28	Mg–Zn–Ca	Asymmetric	$Ca(NO_2)_2$	6.9	Ca–P with	[24]
		pulses.	NH ₄ H ₂ PO ₄	2.88	atomic ratio	[[- ·]
		$i_{c}/i_{a}=2$:	NaNO ₃	13.9	1.33:1.65	

		$i_a 100 A.m^2$	HNO ₃			
		t=30 min	(CH ₂ OH) ₃ CNI	H ₂),		
			NH ₄ OH adj	justing		
			pH =5			
		Bo	orate electrolyte	s		
29	AZ31,	Alternative	NaOH	50	MgO	[26]
	AZ91D	current,	H ₃ BO ₃	10		
		120 V	$Na_2B_4O_710H_2O_7$	O 20		
		$t=3 \min$	C ₆ H ₅ O ₇ Na ₃	10		
			$Na_2WO_4 2H_2O_4$) ₈		
			А			
			(organic additi	ve) 2		

Electrolytes for PEO treatment of AZ31 alloy were classified according to their pH [27] (Table. 3).

Table 3. Electrolytes for PEO of alloy AZ31

	Silicate electrolytes (mol.L ⁻¹)	pH				
1	$0.035Na_2SiO_3+0.07KOH (M_{Na}:M_K=1:1)$	12.99				
2	$0.07Na_2SiO_3+0.07KOH (M_{Na}:M_K=2:1)$	12.91				
3	0.07Na ₂ SiO ₃ +0.07KOH+0.085KF+ glycol	12.96				
4	$0.07 \operatorname{Na_2SiO_3}$	12.7				
5	$0.07Na_2SiO_3 + KOH(\rho = 32 \text{ mS.cm}^{-1})$	13.3				
	Phosphate electrolytes (mol. L^{-1})					
6 ¹	$H_{3}PO_{4}+K_{2}ZrF_{6}^{2}$ (M $_{H3PO4}$: M $_{K2ZrF6}=1:9$)	2.33				
7	NaH ₂ PO ₄ +K ₂ ZrF ₆ (M _{NaH2PO4} : M _{K2ZrF6} =1:9)	3.68				
8	$Na_2HPO_4+K_2ZrF_6$ (M _{Na2HPO4} : M _{K2ZrF6} =1:9)	5.73				
9	Na ₅ P ₃ O ₁₀ +K ₂ ZrF ₆ (M _{Na5P3O10} : M _{K2ZrF6} =1:9)	9.46				
10	0.07 Na ₃ PO ₄	12.45				
11	$0.07 \text{ Na}_{3}\text{PO}_{4} + \text{KOH} (\rho = 32 \text{ mS.cm}^{-1})$	13.38				
	Aluminate electrolytes (mol.L ⁻¹))				
12	0.07 NaAlO ₂	12.46-12.50				
13	$0.07 \text{ NaAlO}_2 + \text{KOH}(\rho = 32 \text{ mS.cm}^{-1})$	13.30				
Others (mol L^{-1})						
14	0.07 KF	9.08				
15	$0.07 \text{ KF+KOH} (\rho = 32 \text{ mS.cm}^{-1})$	13.18				
16	$0.07Na_2B_4O_7 + KOH (\rho = 32 \text{ mS.cm}^{-1})$	13.01				
17	$0.07Na_2CO_3 + KOH (\rho = 32 \text{ mS.cm}^{-1})$	13.04				
18	0.69 KOH	14.00				

²The molar concentration of K_2ZrF_6 was 0.025; the content of K_2ZrF_6 in the reagent exceeded 98% by weight.

The structure of the coatings is determined by five main factors: chemical composition of the electrolyte and the alloy, current density, electrical processing regime and duration of the process. As a rule, the surface of PEO coatings has a fairly coarse porous structure and needs subsequent removal of the top layer, or to be sealed. It was considered [12] that spherical pores of PEO coating surrounded by a halo of fused material are formed by outgoing gases. So, any measures limiting gas generation at the electrode and contributing to a decrease in temperature on the surface of the coating will positively affect the morphology of the surface.

It was found [28] that the coatings obtained from silicate (10 g.L⁻¹ Na₂SiO₃ + 1 g.L⁻¹ KOH) and phosphate (10 g.L⁻¹ Na₃PO₄ + 1 g.L⁻¹ KOH) electrolytes by the pulses with equal anodic and cathodic current densities 600 A.m⁻² were slightly different. At the same time, the "phosphate" coating had a more compact and continuous structure than the "silicate" one.

There are indirect data about the positive influence of magnesium fluoride on the structure and morphology of PEO coatings [29]. The introduction of fluorides in magnesium oxide at the high temperature ($635 - 705^{\circ}$ C) treatment in SF₆ atmosphere was found. Fluorine particles diffused through the oxide layer and formed magnesium fluoride in the interphase space between the metal and the oxide film. In some cases, a layer enriched in fluoride was detected between the oxide crystals. It has been suggested that magnesium fluoride increases the Pilling-Bedworth ratio of Mg/MgO to 1 due to incorporation into the oxide structure.

3. Corrosion resistance

A comparative characteristic of anticorrosive coatings on magnesium is given in [30]. The total corrosion rate was determined by immersion in 3.5% (by weight) NaCl solution at 20° C for 48 hours. The protective ability was carried out by results of salt spray tests after 336 hours of exposure in accordance with ASTMB893-98 (Table 4).

Process	Electrolyte	Regime	Thickness	Average	Defensive
			(µm)	corrosion	ability (score)
				rate	
				$(mg.m^{-2}.h^{-1})$	
Bare				257.97	0
Mg					
HAE	КОН,	$t=15-30^{\circ}C$	19	148.82	2-3
	Al(OH) ₃ ,	U=70-90 V			
	KF,	I(~)=20-25			
	Na ₃ PO ₄ ,	τ=8-60 min			
	KMnO ₄				
DOW17	NH ₄ HF ₂ ,	$t=71-82^{0}C$	31	221.81	7-8
	$Na_2Cr_2O_7$,	U=70-90 V			
	H_3PO_4	I(~/-)=5-50			
		$mA.cm^{-2};$			
		τ=5-25 min			
PEO	КОН,	$t=885^{\circ}C$	10	49.85	7-8
(silicate-	Na ₂ CO ₃ ,	U=150 V	17	42.16	>8
borate)	Na ₂ SiO ₃ ,	I(~/-)=5-500	33	32.54	9
	$Na_2B_4O_7$	$mA.cm^{-2};$			
		t=10-80 min			

Table 4. Corrosion resistance of the coatings on magnesium

It was mentioned above that the stability of the protective oxide/hydroxide layer MgO/Mg $(OH)_2$ is observed at pH 11.46 – 13.83. Reducing the pH to 7.4, for example, in biological media, leads to a slow dissolution of the oxide [31]:

$$MgO + 2H^+ \rightarrow Mg^{2+} + H_2O$$
 (1)

$$Mg(OH)_2 + 2H^+ \rightarrow Mg^{2+} + 2H_2O$$
⁽²⁾

In the corrosion media with Cl⁻ions magnesium forms soluble salt MgCl₂.

The optimization of PEO parameters to obtain corrosion-resistant coatings on AM50 alloy was carried out by Taguchi method [32]. It turned out that between variations of current density, time of electrolysis and electrolyte composition (KOH, NaAlO₂), the concentration of alkali was of decisive importance. The optimal process values were found such as: current density 1200 A.m⁻², time of electrolysis 12 min, KOH and NaAlO₂ concentrations 9 and 15 g.L⁻¹ respectively.

4. Sealing of PEO coatings

The main disadvantage of PEO coatings for anticorrosion ability is their porosity [33]. As usual, porous anodic films are sealed by soaking in hot water with additives of potassium dichromate [34]. This method is not applicable for PEO coatings because of their hydrophobicity. The nonequilibrium vitrified surface of films obtained under sparking followed by quenching in a cold electrolyte cannot be stabilized in hot water.

The best way to stabilize the nonequilibrium phases on the surface is to calcine the coatings, but the temperature regime should be carefully followed, taking into account the very complex mechanism of hydroxide dehydration and the relatively low melting temperature of the metal substrate (650° C). The thermal treatment of coatings in the range of $50 - 250^{\circ}$ C, leading to the dehydration of Mg(OH)₂ and Al(OH)₃ and their transition to MgO and Al₂O₃ oxides is quite effective. Calcination at 150° C followed by air cooling significantly increased the corrosion resistance of the AZ91D alloy in 3.5% NaCl [35].

The method of filling PEO coatings on magnesium which used in commercial processes Magoxid-Coat® and Tagnite®, has been described in [36]. Immediately after oxidation in the aluminate-phosphate electrolyte, the samples were immersed for 5 min in an alkaline phosphate solution (12% NaH₂PO₄) at 60^oC, or for 15 min in a silicate solution (5%) at 95^oC. The samples were then thoroughly washed and dried. As a result of this treatment, the overall thickness and porosity of the coatings were reduced. The silicate solution appeared to be more effective than the phosphate solution.

Dense corrosion-resistant coatings on the AM50B and AM60B alloys were obtained after sealing of PEO coatings with a sol-gel method. To prepare the sol-gel solution, 14 ml of tetraethylorthosilicate (TEOS) and 2% by weight of methyl-triethoxysilane (MTES) were dissolved in 2 ml of high purity ethanol. The solution was hydrolysed by adding H₂O (2.5 ml) acidified with 0.35 ml HCl and stirred for 1 hour. Hydrochloric acid served as a catalyst for hydrolysis and polycondensation reactions, and also prevented the agglomeration of particles. After electrolysis, the samples were immersed in the mixture for 1 minute, slowly removed, then held for 3 hours at 160° C and cooled in air. The procedure was repeated three times then samples were washed for 3 min by distilled water and dried 24 hours at room temperature.

The similar technology was used for filling PEO coatings on an AZ91D alloy [37]. The silica sol (0 – 30% by volume) was added to the silicate electrolyte (1M Na₂SiO₃). The sol was prepared from tetraethoxysilane (TEOS), methyl triethoxysilane (MTES). Water (pH = 2, adjusted with 0.1 mol.L⁻¹ H₂SO₄) and ethanol

were taken in molar ratios of 1:2:10:15, respectively. The components were mechanically stirred for 1 hour and held for 5 hours at 60° C.

The reactions underlying the formation of the gel are given below:

$$Si - O - R + H_2O \rightarrow Si - OH + R - OH$$
(hydrolysis) (3)

$$Si - OH + HO - Si \rightarrow Si - O - Si + H_2O$$
 (condensation of water) (4)

 $Si - O - R + HO - Si \rightarrow Si - O - Si + R - OH$ (condensation of alcohol) (5) A significant improvement in the corrosion resistance of coatings was observed even at a sol concentration of 10% by volume.

The application of sol-gel over the PEO films obtained from the aluminate electrolyte was reported in [38]. The gel was prepared by mixing 3-methacryloxypropyl-trimethyloxysilane (MEMO, 99.97%, 19.8 g), 3-mercaptopropyl trimethoxysilane (TPTMS, 95%, 0.8 g) and ethanol (95%, 0.8 g). Then, colloidal silica (9 g) was added dropwise to the mixture while stirring. After hydrolysis of the mixture, an oligomer (6.8 g) and a photo initiator (2-hydroxyl-2-methylpropiophene, 2 g) were added thereto. The sol was diluted with alcohol to obtain an appropriate viscosity and applied to the oxide by spraying (up to 5 layers). The samples were then irradiated with ultraviolet and thermally treated at 1500 ° C for 30 min. Optimal results in electrochemical corrosion tests in 3% NaCl were obtained by applying two sol-gel layers (15 μ m each).

The application of tetrafluoroethylene should be considered as a productive method of sealing the PEO surface layer. The application of organic substance above PEO coating was described in [39]. Coatings were immersed in the solution for 1 min, followed by vulcanization at 50° C for 30 min. The thickness of the sealing layer with this treatment reached 2 μ m. For qualitative filling of pores and defects, the process was repeated two to three times.

5. Conclusion

PEO technology is suitable for treatment of different Mg alloys to obtain oxide (MgO), hydroxide Mg(OH)₂, and different chemical compounds sintered from the electrolyte (MgAl₂O₄, Mg₂SiO₄, Mg₃(PO₄)₂) in crystalline and amorphous forms. Today, the most qualitative and homogeneous coating can be formed in silicate electrolytes at the high frequency bipolar pulse mode but there are no clear evidences of significant advantages of any used technologies. The better results can be obtained by adding fluoride in the electrolyte. PEO coatings possess a coarse porous structure and relatively poor mechanical properties which can be partly eliminated by following filling.

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